Neural Network Approach for Estimation of Penetration Depth in Concrete Targets by Ogive-nose Steel Projectiles

Abstract

Despite the availability of large number of empirical and semi-empirical models, the problem of penetration depth prediction for concrete targets has remained inconclusive partly due to the complexity of the phenomenon involved and partly because of the limitations of the statistical regression employed. Conventional statistical analysis is now being replaced in many fields by the alternative approach of neural networks. Neural networks have advantages over statistical models like their data-driven nature, model-free form of predictions, and tolerance to data errors. The objective of this study is to reanalyze the data for the prediction of penetration depth by employing the technique of neural networks with a view towards seeing if better predictions are possible. The data used in the analysis pertains to the ogive-nose steel projectiles on concrete targets and the neural network models result in very low errors and high correlation coefficients as compared to the regression based models.

Keywords

Neural Networks; penetration depth; concrete targets; projectile.

M. Hosseini[a]
A. Dalvand[b]

[a]Dept. of Civil Engineering, Lorestan University, Khoramabad, P.O. Box 465, Iran.
[b]Dept. of Civil Engineering, Lorestan University, Khoramabad, Iran.

Corresponding autor:
[a]mo_hosseini78@yahoo.com
[b]alidalvand85@yahoo.com

1 INTRODUCTION

Concrete has been widely used over many years by military and civil engineers in the design and construction of protective structures to resist impact and explosive loads. Potential missiles include kinetic munitions, vehicle and aircraft crashes, fragments generated by military and terrorist bombing, fragments generated by accidental explosions and other events (e.g. failure of a pressurized vessel, failure of a turbine blade or other high-speed rotating machines), flying objects due to natural forces (tornados, volcanos, meteoroids), etc. These missiles vary broadly in their sizes and shapes, impact velocities, hardness, rigidities, impact attitude (i.e. obliquity, yaw, tumbling, etc.) and produce a wide spectrum of damage in the target (Li et al., 2005).

In the past 60 years, a large amount of laboratory tests had been conducted in various countries (Kennedy, 1976; Sliter 1980; Williams, 1994; Corbett et al., 1996). Based on these available

test data, empirical formulae have been proposed to predict the penetration depth on concrete target. Empirical formulae on penetration depth, perforation limit and scabbing limit in a thick concrete target had been reviewed by Kennedy (1976), which covered most of the test data in the US and European till 1970s. Comparison between various empirical formulae and published test data was conducted by Williams (1994). Among the most commonly used formulae are the Pettry formula, the Army Corps of Engineers formula (ACE), Ballistic Research Laboratory formula (BRL) and the National Defence Research Committee (NDRC) formula.

In this study, by using the projectile and target parameters, proposed a dimensionless empirical formula to predict the rigid projectile penetration depth of concrete target. It is shown that these dimensionless formula is capable of representing test data on penetration depth in a broad range of impact velocity as long as the projectile deformation is negligible, which covers the applicable range of empirical formulae.

2 AVAILABLE FORMULA FOR LOCAL CONCRETE DAMAGE PREDICTION

The most commonly formula used to predict various components of local impact effects of hard missile on concrete structure in USA was modified Petry formula. It is the oldest of available empirical formulae, and developed originally in 1910. According to Petry the penetration depth x (inches) can be predicted as (Kennedy, 1976):

$$x = 12K_p A_p \log_{10}\left(1 + \frac{V^2}{215000}\right) \tag{1}$$

This equation was derived from the equation of motion which states that the component of drag-resisting force depends upon square of the impacted velocity, and the instantaneous resisting force is constant. In above equation, A_p represents the missile section pressure (psi). K_p is concrete penetrability coefficient, it depends upon the strength of concrete and on the degree of reinforcement. It equals to 0.00426 for normal reinforced cement concrete, 0.00284 for special reinforced cement concrete (front and rear face reinforcement are laced together with special ties), and 0.00799 for massive plain cement concrete.

Before 1943, The Ordnance Department of the US Army and Ballistic Research Laboratory (BRL) done many experimental works on local impact effects of hard missile on concrete structure, based on those results Army Corp of Engineers developed the ACE formula (Kennedy, 1976; Chelapati et al., 1972; ACE 1946):

$$\frac{x}{d} = \frac{282.6}{\sqrt{f_c}}\left(\frac{W}{d^3}\right)d^{0.215}\left(\frac{V}{1000}\right)^{1.5} + 0.5 \tag{2}$$

For the calculation of penetration depth (x) of concrete impacted by hard missile, Ballistic Research laboratory (BRL) was suggested a formula in 1941 (Beth, 1941; Chelapati et al., 1972), and its modified expression was given by Kennedy (1976); Adeli et al. (1985):

$$\frac{x}{d} = \frac{427}{\sqrt{f_c}} \left(\frac{W}{d^3} \right) d^{0.2} \left(\frac{V}{1000} \right)^{1.33} \tag{3}$$

Modified National Defense Research Committee (NDRC) Formula: In 1946, the National Defense Research Committee (NDRC) proposed the following formula for predicting the penetration depth (Kennedy, 1976; NDRC 1946; Kennedy, 1966):

$$\frac{x}{d} = \left(4NKW \frac{V}{d} \left(\frac{V}{1000d} \right)^{1.8} \right)^{0.5} \quad \text{for } \frac{x}{d} \le 2 \tag{4}$$

$$\frac{x}{d} = 1 + \frac{NKW}{d} \left(\frac{V}{1000d} \right)^{1.8} \quad \text{for } \frac{x}{d} \ge 2 \tag{5}$$

K is the concrete penetration factor and is given as a function of concrete strength f_c as follows:

$$K = \frac{180}{\sqrt{f_c}} \tag{6}$$

N is the missile nose shape factor. 1.0 For average bullet nose (spherical end), 0.84 for blunt nosed bodies and 1.14 for very sharp nose. All the above empirical formula applied only for non-reinforced structures impacted by solid missile.

Ammann and Whitney (A&W) formula was proposed to predict penetration of concrete target against the impact of explosively generated small fragments at relatively higher velocities. According to Kennedy (Kennedy, 1976) this formula can predict penetration of explosively generated small fragments traveling at over 1000 ft/sec.

$$\frac{x}{d} = \frac{282}{\sqrt{f_c}} N^* \left(\frac{M}{d^3} \right) d^{0.2} \left(\frac{V}{1000} \right)^{1.8} \tag{7}$$

In this formula N^* is the nose shape function same as defined in NDRC formula.

Where in the above equations:
d is the diameter of the missile in inches
W is the weight of the missile in pounds
f_c is the compressive strength of concrete in Psi
And V missile velocity in ft/sec^2

Haldar – Hamieh (Halder and Hamieh, 1984) suggested the use of an impact factor I_a, defined by:

$$I_a = \frac{MN^*V^2}{f_c d^3} \tag{8}$$

where I_a is impact factor and it is a dimensionless term, N^* is the nose shape factor defined in the modified NDRC formula. For penetration depth (x):

$$\frac{x}{d} = 0.2251I_a + 0.0308 \quad \text{for } 0.3 \leq I_a < 4.0 \tag{9}$$

$$\frac{x}{d} = 0.0567I_a + 0.674 \quad \text{for } 4.0 \leq I_a < 21 \tag{10}$$

$$\frac{x}{d} = 0.0299I_a + 1.1875 \quad \text{for } 21 \leq I_a < 455 \tag{11}$$

Li and Chen (Li and Chen, 2003) further develop Forrestal et al. (1994) model and proposed semi – empirical or semi – analytical formulae for the penetration depth (x). The formulae are in dimensional homogenous form, and defines nose shape factor analytically.

$$\frac{x}{d} = \sqrt{\frac{(1 + (k\pi/4N))}{1 + I/N} \cdot \frac{4kI}{\pi}} \quad \text{for } \frac{x}{d} \leq 5 \tag{12}$$

$$\frac{x}{d} = \frac{2}{\pi} N \ln \left[\frac{1 + (I/N)}{1 + (k\pi/4N)} \right] + k \quad \text{for } \frac{x}{d} > 5 \tag{13}$$

Where

$$I = \frac{1}{S} \left(\frac{MV^2}{f_c d^3} \right) \tag{14}$$

$$N = \frac{1}{N^*} \left(\frac{M}{\rho_C d^3} \right) \tag{15}$$

where N, I, and N^* are the impact function and the geometry function and nose shape factor respectively. S is an empirical function of fc (MPa) and is given by:

$$S = 72f_c^{-0.5} \tag{16}$$

The above equations are applicable for $x/d \geq 0.5$, and reduced the results obtained by Forrestal et al. (1996) for an ogive – nose projectile. Forrestal et al. (1994, 1996) and Frew et al. (1998) suggested that if $x/d \geq 5.0$ than $k = 2.0$, this statement is strengthened by the instrumented experiments in (Forrestal et al. 2003), and with penetration experiments with wide range of projectile diameter (Frew et al. 2000) And Li and Chen (2003) recommended $x/d < 5.0$, for small – to – medium penetration depths:

$$k = \left(0.707 + \frac{h}{d} \right) \tag{17}$$

where h is the length of nose of the projectile and d is the diameter of the projectile.

3 EXPERIMENTAL DATA

The data used in the analysis is taken from Frew et al. (1998); Forrestal et al. (1994); Forrestal et al. (1996); Forrestal et al. (2003) which makes a total of 70 data points. The data consists of four parameters viz. projectile diameter (d), projectile velocity (V), compressive strength of concrete (f_c), projectiles weight (W). The range of these parameters for the data is given in Table 1.

S. NO.	Parameter	Range
	Basic Parameters	
1	Projectile diameter, d (mm)	12.9 - 76.2
2	Projectile velocity, V (m/s)	139.3 - 1225
3	Projectile weight (N)	0.63 - 129
4	compressive strength of concrete f_c (MPa)	13.5 - 62.8
	Non-Dimensional Parameters	
1	$MV^2 \big/ Sf_c d^3$	$1.66 - 164.06$

Table 1: Range of parameters for the data of experimental details of projectiles and concrete targets (70 data points).

4 PROPOSED MODEL

The empirical model used for the prediction of penetration depth in concrete target is:

$$\frac{x}{d} = C_1 \left(\frac{MV^2}{Sf_c d^3} \right)^{C_2} + C_3 \tag{18}$$

Where, C_1, C_2, C_3 are the model parameters, M is projectiles mass and S is an empirical function of fc (MPa) and is given by (Forrestal et al., 1996):

$$S = 82.6 f_c^{-0.544} \tag{19}$$

Parameters C_1 to C_3, have been determined by regression analysis for data involving (a) projectiles with CRH=3 to 4.25 and (b) projectiles with CRH= 6. Thus giving tow regression models:

$$\frac{x}{d} = \left(\frac{MV^2}{Sf_c d^3} \right)^{0.85} + 1 \quad \text{for projectiles with CRH=3 to 4.25} \tag{20}$$

$$\frac{x}{d} = 1.6 \left(\frac{MV^2}{Sf_c d^3} \right)^{0.85} + 1 \quad \text{for projectiles with CRH= 6} \tag{21}$$

Where (CRH) is caliber-radius-head of the projectiles.

The performance of various regression models presented above has been compared in Table 2 with the help of mean percentage error. It is observed from this table that the mean error of Proposed model is lower than other models.

Number of data	Mean Percentage Error %							
	BRL	ACE	NDRC	Li&Chen	A&W	Pettry	Halder	Eqs. (20)-(21)
70	16.3	28.2	31.7	12.6	12	99.2	56	10.3

Table 2: Mean percentage error for different models.

5 NEURAL NETWORK MODEL

The manner in which the data are presented for training is the most important aspect of the neural network method. Often this can be done in more than one way, the best configuration being determined by trial-and-error. It can also be beneficial to examine the input/output patterns or data sets that the network finds difficult to learn. This enables a comparison of the performance of the neural network model for these different combinations of data. In order to map the causal relationship related to the penetration depth, two separate input-output schemes (called Model – A1 and Model – A2) were employed, where the first took the input of raw causal parameters while the second utilized their non-dimensional groupings. This was done in order to see if the use of the grouped variables produced better results? The Model – A1 thus takes the input in the form of causative factors namely, W, V, d, and f_c yields the output, the penetration depth, x, while Model – A2 employs the input of grouped dimensionless variables namely, $MV^2 \big/ Sf_c d^3$, and yields the corresponding dimensionless output x/d . Thus, the two models are:

$$\text{Model – A1:} \quad x = f\left(W, V, d, f_c\right) \tag{22}$$

$$\text{Model – A2:} \quad \frac{x}{d} = f\left(\frac{MV^2}{Sf_c d^3}\right) \tag{23}$$

The input and output variables involved in the above two models were first normalized within the range 0 to 1 as follows:

$$x_N = \frac{x - x_{\min}}{x_{\max} - x_{\min}} \tag{24}$$

Where x_N is the normalized value of x; $x_{\max}$ and $x_{\min}$ are the maximum and minimum values of variable, x. This normalization allowed the network to be trained better.

The current study used the data considered above (70 data points) for the prediction of penetration depth. The training of the above two models was done using 67% of the data (46 data points) selected randomly. Validation and testing of the proposed models was made with the help

of the remaining 33% of observations (24 data points), which were not involved in the derivation of the model.

Three neuron models namely, tansig, logsig and purelin, have been used in the architecture of the network with the back-propagation algorithm. In the back-propagation algorithm, the feed-forward (FFBP) and cascade-forward (CFBP) type network was considered. Each input is weighted with an appropriate weight and the sum of the weighted inputs and the bias forms the input to the transfer function. The neurons employed use the following differentiable transfer function to generate their output:

Log-Sigmoid Transfer Function: $\quad y_j = f\left(\sum_i w_{ij} x_i + \varphi_j\right) = \dfrac{1}{1 + e^{-\sum w_{ij} x_i + \varphi_j}}$ $\qquad$ (25)

Linear Transfer Function: $\qquad y_j = f\left(\sum_i w_{ij} x_i + \varphi_j\right) = \sum_i w_{ij} x_i + \varphi_j$ $\qquad$ (26)

Tan-Sigmoid Transfer Function: $\quad y_j = f\left(\sum_i w_{ij} x_i + \varphi_j\right) = \dfrac{2}{1 + e^{-2\sum w_{ij} x_i + \varphi_j}} - 1$ $\qquad$ (27)

The weight, w, and biases, φ, of these equations are determined in such a way as to minimize the energy function. The Sigmoid transfer functions generate outputs between 0 and 1 or -1 and +1 as the neuron's net input goes from negative to positive infinity depending upon the use of log or tan sigmoid. When the last layer of a multilayer network has sigmoid neurons (log or tan), then the outputs of the network are limited to a small range, whereas, the output of linear output neurons can take on any value.

Further, in order to see if advanced training schemes provide better learning than the basic back propagation, a radial basis function (RBF) network was also used which though requires more neurons but it is sometimes more efficient. The Radial basis transfer function is given by:

$$y_j = f\left(\sum_i \|w_{ij} - x_i\| \varphi_j\right) = e^{-\sum \|w_{ij} - x_i\| \varphi_j^2} \qquad (28)$$

The optimal architecture was determined by varying the number of hidden neurons. The optimal configuration was based upon minimizing the difference between the neural network predicted value and the desired output. In general, as the number of neurons in the layer is increased, the prediction capability of the network increases in beginning and then becomes stationary.

The performance of all neural network model configurations was based on the Mean Percent Error (MPE), Mean Absolute Deviation (MAD), Root Mean Square Error (RMSE), Correlation Coefficient (CC), and Coefficient of Determination, R^2, of the linear regression line between the predicted values from the neural network model and the desired outputs.

The training of the neural network models was stopped when either the acceptable level of error was achieved or when the number of iterations exceeded a prescribed maximum. The neural network model configuration that minimized the MAE and RMSE and optimized the R^2 was selected as the optimum and the whole analysis was repeated several times.

6 SENSITIVITY ANALYSIS

Sensitivity tests were conducted to determine the relative significance of each of the independent parameters (input neurons) on the penetration depth (output) in both of the models given by Eqs. (22) and (23). In the sensitivity analysis, each input neuron was in turn eliminated from the model and its influence on prediction of penetration depth was evaluated in terms of the MPE, MAD, RMSE, CC and R^2 criteria. The network architecture of the problem considered in the present sensitivity analysis consists of one hidden layer with thirteen neurons for model-A1and fourteen neurons for model-A2 and the value of epochs has been taken as 100.

The comparison of different neural network models, with one of the independent parameters removed in each case is presented in Table 3. The influence of the removal of one independent parameter at a time has been studied for all four parameters. The results in Table 3 show that for Model – A1, the velocity of projectile, V, and compressive strength of concrete, f_c , are the two most significant parameters for the prediction of penetration depth. The variables in the order of decreasing level of sensitivity for Model – A1 are: V, f_c, d and W.

Input variables	MPE	MAD	RMSE	CC	R^2
All Eq.(22)	-0.34	5.1	5.01	0.996	0.992
No V	-11.7	55.5	52.4	0.610	0.2
No W	-0.26	5.0	8.3	0.980	0.97
No d	0.51	5.1	5.4	0.988	0.98
No f_c	2.4	8.7	12.4	0.970	0.95

Table 3: Sensitivity analysis for Model –A1 with Feed Forward Back Propagation.
Note: MPE = Mean Percent Error; MAD = Mean Absolute Deviation; RMSE = Root Mean Square Error; CC = Correlation Coefficient; R^2 = Coefficient of Determination.

Input	MPE	MAD	RMSE	CC	R^2
Eq.(23)	3.25	9.6	3.5	0.988	0.978

Table 4: analysis results for Model–A2 with ANN.

7 NUMERICAL RESULTS

As dictated by the use of Gaussian function all patterns were normalized within range of 0.0 to 1.0 before their use. Similarly all weights and bias values were initialized to random numbers. While the numbers of input and output nodes are fixed, the hidden nodes in the case of FFBP were subjected to trials and the one producing the most accurate results (in terms of the Correlation Coefficient) was selected. The optimization of the training procedure automatically fixes the hidden nodes in the case of the CFBP. The training of these networks was stopped after reaching the minimum mean square error between the network yield and true output over all the training patterns. For the RBF network various values of spread between 0 and 1 were tried out and the one of 0.01 resulting in the best performance on both training and testing data was selected.

The information on number of nodes required to achieve minimum error taken in the case of each training scheme used (i.e. FFBP, CFBP, and RBF) is shown in Table 5 for Model –A1 and A2. As a matter of general information, which is not of real significance in this study, it can be seen that the cascade correlation algorithm, designed for efficient training, trained the network with fewer epochs than the FFBP network, but the RBF network was trained in a significantly less number of epochs, indicating its training efficiency.

Model	Algorithm	Network Configuration			Learning Rate	Momentum Function
		I	H	O	0.5	0.7
	FFBP	4	13	1	0.5	0.7
Model – A1	CFBP	4	15	1	0.5	0.7
	RBF	4	60	1	0.5	0.7
	FFBP	1	14	1	0.5	0.7
Model - A2	CFBP	1	17	1	0.5	0.7
	RBF	1	55	1	0.5	0.7

Table 5: Network Architecture.
Note: *I, H, O* indicate number of input, hidden, and output nodes, respectively; FFBP = Feed-Forward Back Propagation; CFBP = Cascade-Forward Back Propagation; and RBF = Radial Basis Function.

The network architecture of the two models, given by Eqs. (22)-(23), is given in Figs. 1-2 respectively for BP/RBF training scheme. The error estimation parameters (MPE, MAD, RMSE, CC and R^2), on the basis of which the performance of a model is assessed, are already given in Tables 3-4.
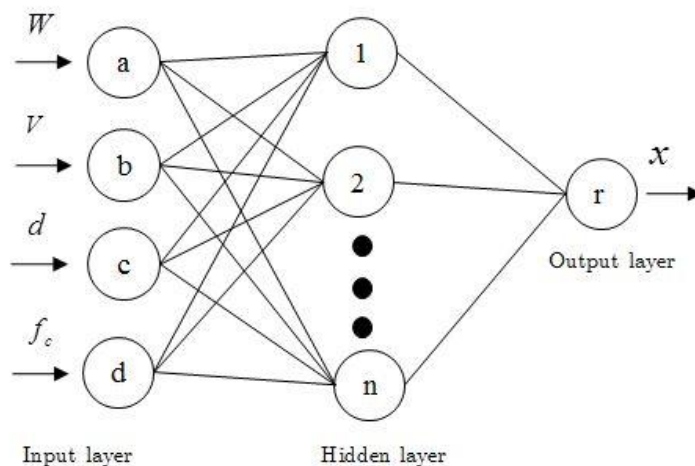

Figure 1: Model—A1: use of raw variables.

The training and validation of the two models is shown in Figs. 3-4. The trained values of connecting weights and bias for the two models are given in Tables 6-7 obtained from FFBP training scheme.
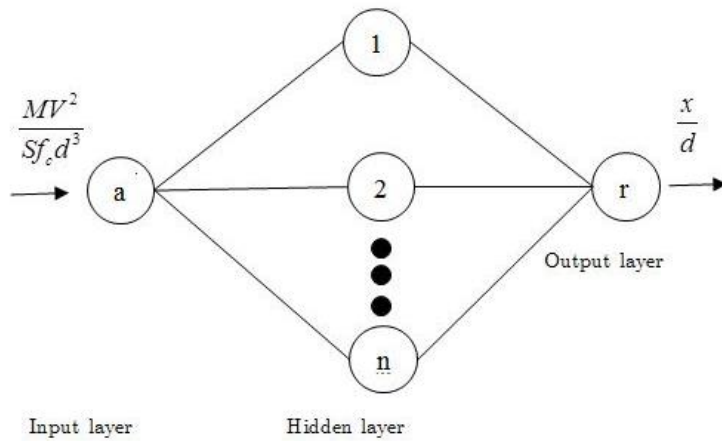
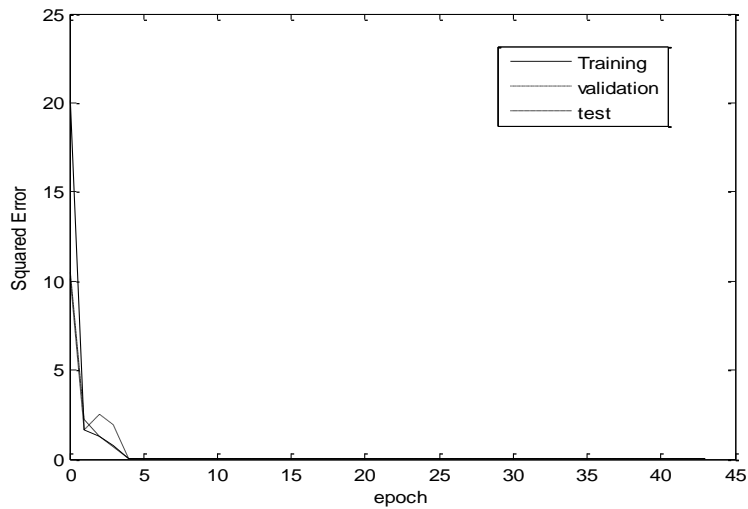Figure 2: Model—A2: use of grouped variables

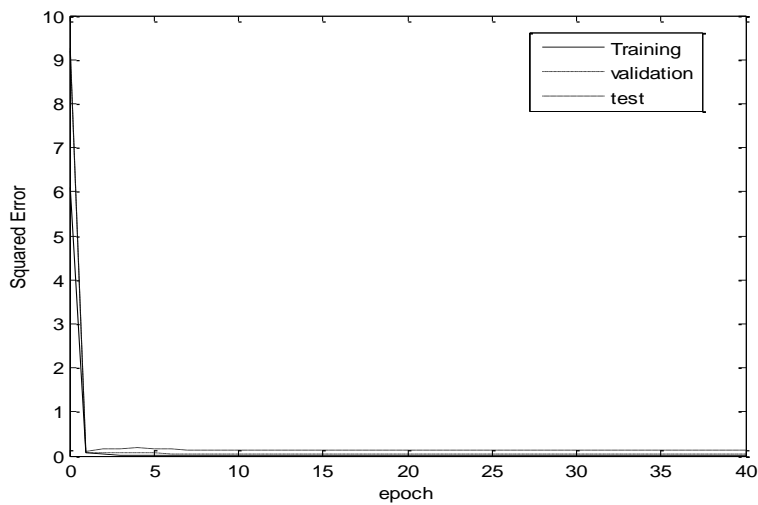Figure 3: Epochs versus squared error of raw variables by back propagation.

Figure 4: Epochs versus squared error of grouped variables by back propagation.

No. of neuron	Input weights				Output weights	Input biases
	a	b	c	d	r	
1	-1.83	-2.107	-0.41	1.1	1.6991	2.4981
2	1.83	1.17	0.83	0.9	-1.9403	-0.7743
3	-0.34	1.78	2.17	-0.3	0.0503	1.6994
4	-1.73	0.49	-1.39	-1.6	-0.71	0.3887
5	1.18	2.26	-0.66	-0.04	-0.852	-0.9643
6	-0.69	-0.97	-2.45	0.66	-0.438	0.3199
7	0.56	-1.06	-1.81	1.05	-0.3551	0.3068
8	2.48	1.61	0.89	1.52	1.6615	0.1549
9	-0.89	-1.48	-1.395	1.084	0.4994	-1.0383
10	1.25	-1.39	0.9	-1.09	0.4744	0.5866
11	-4	-1.41	0.084	-0.888	-1.0161	-0.168
12	1.859	0.2271	-2.37	4.16	0.4721	1.5101
13	0.298	0.968	0.073	1.92	0.0715	-3.0808

Table 6: Connection weights and biases (Refer to Figure 1).
(Output bias= -1.6).

No. of neuron	Input weights	Output weights	Input biases
	a	r	
1	20.015	-1.444	-19.197
2	-19.5954	-1.2504	16.8313
3	-19.1899	0.0419	14.1144
4	-20.1306	-0.0974	9.3933
5	19.4844	-0.0327	-7.9381
6	-20.0332	-0.0863	4.517
7	-19.7706	-0.1156	2.1064
8	-19.4814	-0.1696	-2.9871
9	19.8566	-0.0404	3.2438
10	-19.6182	-0.12	-7.6026
11	18.8785	0.255	12.0185
12	-19.8142	0.137	-13.210
13	-19.6967	-0.0704	-16.386
14	-19.5918	-0.0855	-19.587

Table 7: Connection weights and biases (Refer to Figure 2).
(Output bias= -0.52).

The percentage error in the prediction of penetration depth for different data sets is plotted in Figs. 5-6 for the two models. The predicted value of penetration depth has been plotted against its observed value in Figs. 7-8 for the two models. Though the results of non-normalized data are not presented but it has been observed that the normalization considerably improved the training of the model.
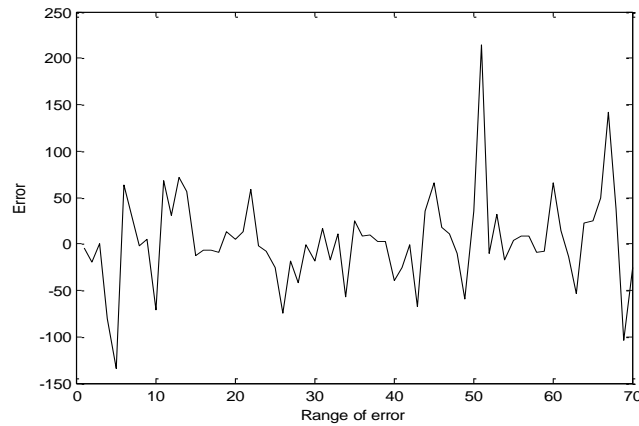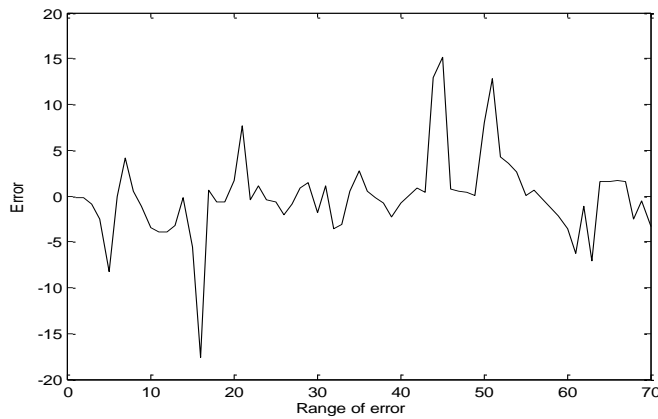
Figure 5: Percentage error for Model-A1.

Figure 6: Percentage error for Model—A2.

The examination of Tables 3-4 and Figs. 7-8 show that when it comes to overall accuracy of predicting penetration depth, all error criteria viewed together point out that the simple feed forward network trained using the common BP algorithm is either as good as or even slightly better than more sophisticated networks.

It also shows that the use of grouped variables as input (Model – A2) may be less beneficial than that of the raw variables (Model – A1), provided an appropriate training scheme is chosen, where perhaps grouping of variables had resulted in evening out their scale effects. The most suitable network, FFBP Model – A1, has the highest CC = 0.996 and R^2 = 0.992; and lowest MPE = –0.34, MAD = 5.1, and RMSE = 5.01. All the ANN models featured small RMSE during training; however, the value was slightly higher during validation. The models showed consistently good correlation throughout the training and testing.

In the end therefore the network configuration (FFBP Model—A1) along with corresponding weight and bias matrix given in Table 6 is recommended for general use in order to predict the penetration depth.

The value of MAD in the prediction of penetration depth by regression model given in Table 2 (10.3% for all data) may be compared with the performance of neural network model—A1 wherein the MAD value is only 5.1%. The histogram of percentage error in the prediction of penetra-

tion depth by regression and the two neural network models is shown in Fig. 9. This clearly indicates the supremacy of the neural network model over the regression model and the one available in literature. Further, the neural networks have advantages over statistical models like their data-driven nature, model-free form of predictions, ability to implicitly detect complex nonlinear relationships between dependent and independent variables, ability to detect all possible interactions between predictor variables and tolerance to data errors.

The predictions should be preferably used within the range of the experimental data because of the possibility of intervention of new phenomena when used beyond the range.
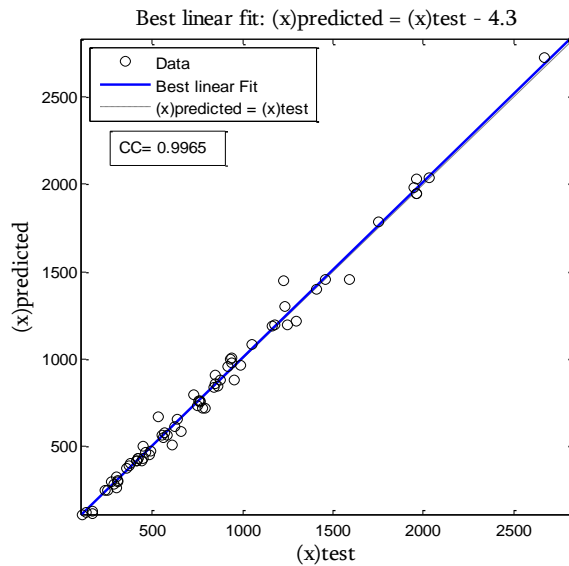
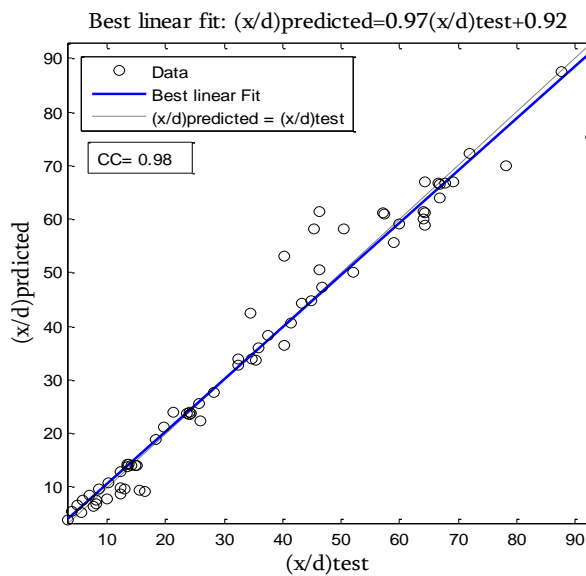Figure 7: Observed versus predicted x (mm) for Model—A1.

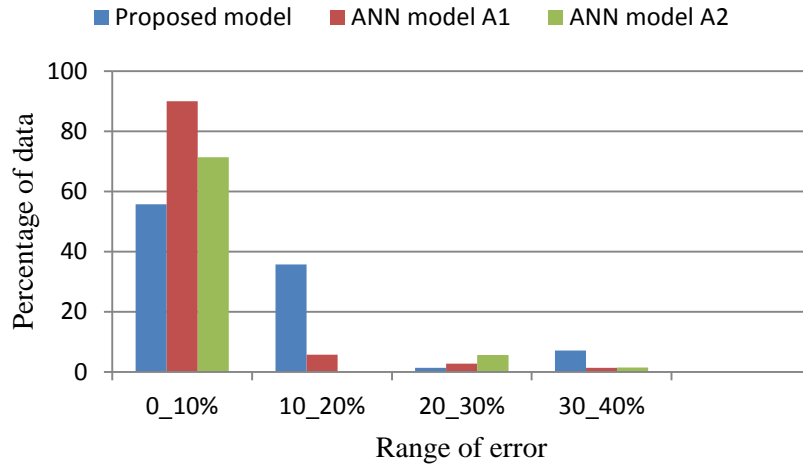Figure 8: Observed versus predicted x/d for Model—A2.

Figure 9: Histogram of percentage error in different models.

8 CONCLUSIONS

A regression based empirical model has been developed based upon the data available in literature for the prediction of penetration depth in concrete target by ogive-nose steel projectiles. The proposed regression model is more accurate predictor of penetration depth than the other available in literature.

Predictions based on the use of raw dimensioned data (V, W, f_c and d) in the development of neural networks were better than those based on the grouped dimensionless forms of the data, $MV^2 / Sf_c d^3$. The neural network with one hidden layer was selected as the optimum network to predict penetration depth. The network configuration of Model – A1 with FFBP is recommended for general use in order to predict the of penetration depth in concrete target by ogive-nose steel projectiles.

The neural network model is far better than the regression based models – proposed as well as the other available in literature for the prediction of the penetration depth in concrete target by ogive-nose steel projectiles.

References

ACE, (1946). Fundamentals of protective structures. Report AT120 AT1207821, Army Corps of Engineers, Office of the Chief of Engineers.

Adeli, H., Amin, A.M., (1985). Local effects of impactors on concrete structures. Nucl. Eng. Des. 88: 301-317.

Beth, R.A., (1941). Penetration of projectiles in concrete. PPAB Interim Report No. 3, November 1941.

Chelapati, C.V., Kennedy, R.P., Wall, I.B., (1972). Probabilistic assessment of hazard for nuclear structures. Nucl. Eng. Des. 19: 333-334.

Corbett, G.G, Reid, S.R, Johnson, W., (1996). Impact loading of plates and shells by free-flying projectiles, a review. Int. J. Impact Eng. 18: 141-230.

Forrestal, M.J., Altman, B.S., Cargile, J.D., Hanchak, S.J., (1994). An empirical equation for penetration depth of ogive-nose projectiles into concrete targets. Int. J. Impact Eng. 15(4): 395-405.

Forrestal, M.J., Frew, D.J., Hanchak, S.J., Brar, N.S., (1996). Penetration of grout and concrete targets with ogive-nose steel projectiles. Int. J. Impact Eng. 18(5): 465-476.

Forrestal, M.J., Frew, D.J., Hickerson, J.P., Rohwer, T.A., (2003). Penetration of concrete targets with deceleration-time measurements. Int. J. Impact Eng. 18: 479-497.

Frew, D.J., Forrestal, M.J., Hanchak, S.J., (2000). Penetration experiments with limestone targets and ogive-nose steel projectiles. ASME J Appl Mech. 67: 841-845.

Frew, D.J., Hanchak, S.J., Green, M.L., Forrestal, M.J., (1998). Penetration of concrete targets with ogive-nose steel rods. Int. J. Impact Eng. 21: 489-497.

Haldar, A., Hamieh, H., (1984). Local effect of solid missiles on concrete structures. ASCE J Struct Div. 110(5): 948-960.

Kennedy, R.P., (1976). A review of procedures for the analysis and design of concrete structures to resist missile impact effects. Nucl. Eng Des. 37: 183-203.

Kennedy, R.P., (1966). Effects of an aircraft crash into a concrete reactor containment building. Anaheim, CA: Holmes & Narver Inc.

Li, Q.M., Chen, X.W., (2003). Dimensionless formulae for penetration depth of concrete target impacted by a non-deformable projectile. Int. J Impact Eng. 28(1): 93-116.

Li, Q.M., Reid, S.R., Wen, H.M., Telford, A.R., (2005). Local impact effects of hard missiles on concrete targets. International Journal of Impact Engineering. 32: 224-284.

NDRC., (1946). Effects of impact and explosión. Summary Technical Report of Division 2, vol. 1, National Defence Research Committee, Washington, DC.

Sliter, G.E., (1980). Assessment of empirical concrete impact formulas. ASCE J. Struct. Div. 106(ST5): 1023-1045.

Williams, M.S., (1994). Modeling of local impact effects on plain and reinforced concrete. ACI Struct. J. 91(2): 178-187.